## Derivation of the Navier-Stokes Equation (Section 9-5, Cengel and Cimbala)

We begin with the general differential equation for conservation of linear momentum, i.e., *Cauchy's equation*, which is valid for any kind of fluid,

Cauchy's equation: 
$$\rho \frac{D\vec{V}}{Dt} = \rho \vec{g} + \vec{\nabla} \cdot (\vec{\sigma}_{ij})$$
 Stress tensor (9–50)

The problem is that the stress tensor  $\sigma_{ij}$  needs to be written in terms of the primary unknowns in the problem in order for Cauchy's equation to be useful to us. The equations that relate  $\sigma_{ij}$ to other variables in the problem – velocity, pressure, and fluid properties – are called *constitutive equations*. There are different constitutive equations for different kinds of fluids.

Types of fluids:



Shear strain rate

## FIGURE 9-37

Rheological behavior of fluids—shear stress as a function of shear strain rate.

Some examples of non-Newtonian fluids:

- Paint (*shear thinning* or *pseudo-plastic*)
- Toothpaste (*Bingham plastic*)
- Quicksand (*shear thickening* or *dilatant*).

We consider only Newtonian fluids in this course.

For *Newtonian fluids* (see text for derivation), it turns out that

$$\sigma_{ij} = \begin{pmatrix} -P & 0 & 0 \\ 0 & -P & 0 \\ 0 & 0 & -P \end{pmatrix} + \begin{pmatrix} 2\mu \frac{\partial u}{\partial x} & \mu \left( \frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \right) & \mu \left( \frac{\partial u}{\partial z} + \frac{\partial w}{\partial x} \right) \\ \mu \left( \frac{\partial v}{\partial x} + \frac{\partial u}{\partial y} \right) & 2\mu \frac{\partial v}{\partial y} & \mu \left( \frac{\partial v}{\partial z} + \frac{\partial w}{\partial y} \right) \\ \mu \left( \frac{\partial w}{\partial x} + \frac{\partial u}{\partial z} \right) & \mu \left( \frac{\partial w}{\partial y} + \frac{\partial v}{\partial z} \right) & 2\mu \frac{\partial w}{\partial z} \end{pmatrix}$$
(9-57)

We have achieved our goal of writing  $\sigma_{ij}$  in terms of pressure *P*, velocity components *u*, *v*, and *w*, and fluid viscosity  $\mu$ .

Now we plug this expression for the stress tensor  $\sigma_{ij}$  into Cauchy's equation. The result is the famous *Navier-Stokes equation*, shown here for incompressible flow. *Incompressible Navier–Stokes equation*:

Navier-Stokes equation: 
$$\rho \frac{DV}{Dt} = -\vec{\nabla}P + \rho \vec{g} + \mu \nabla^2 \vec{V}$$
 (9–60)

To solve fluid flow problems, we need both the continuity equation and the Navier-Stokes equation. Since it is a vector equation, the Navier-Stokes equation is usually split into three components in order to solve fluid flow problems. In Cartesian coordinates, *Incompressible continuity equation*:

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = 0$$
 (9-61a)

*x*-component of the incompressible Navier–Stokes equation:

$$\rho\left(\frac{\partial u}{\partial t} + u\frac{\partial u}{\partial x} + v\frac{\partial u}{\partial y} + w\frac{\partial u}{\partial z}\right) = -\frac{\partial P}{\partial x} + \rho g_x + \mu\left(\frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} + \frac{\partial^2 u}{\partial z^2}\right)$$
(9-61b)

y-component of the incompressible Navier–Stokes equation:

$$\rho\left(\frac{\partial\nu}{\partial t} + u\frac{\partial\nu}{\partial x} + \nu\frac{\partial\nu}{\partial y} + w\frac{\partial\nu}{\partial z}\right) = -\frac{\partial P}{\partial y} + \rho g_y + \mu\left(\frac{\partial^2\nu}{\partial x^2} + \frac{\partial^2\nu}{\partial y^2} + \frac{\partial^2\nu}{\partial z^2}\right)$$
(9-61c)

*z*-component of the incompressible Navier–Stokes equation:

$$\rho\left(\frac{\partial w}{\partial t} + u\frac{\partial w}{\partial x} + v\frac{\partial w}{\partial y} + w\frac{\partial w}{\partial z}\right) = -\frac{\partial P}{\partial z} + \rho g_z + \mu\left(\frac{\partial^2 w}{\partial x^2} + \frac{\partial^2 w}{\partial y^2} + \frac{\partial^2 w}{\partial z^2}\right)$$
(9-61d)