

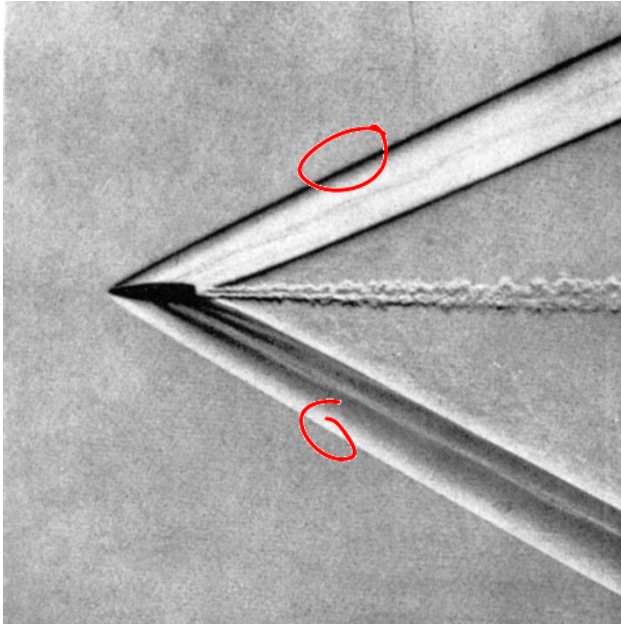
Today, we will:

SO FAR - ONE-DIMENSIONAL FLOWS \star

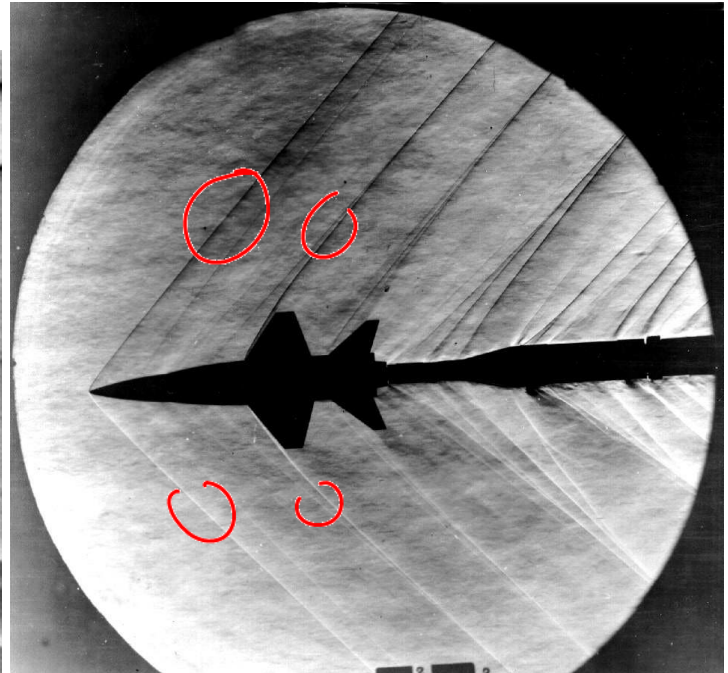
- Discuss *oblique shocks* in two-dimensional compressible flow – *qualitatively* first
- Begin to derive the equations for 2-D oblique shocks

Introduction: Oblique shocks

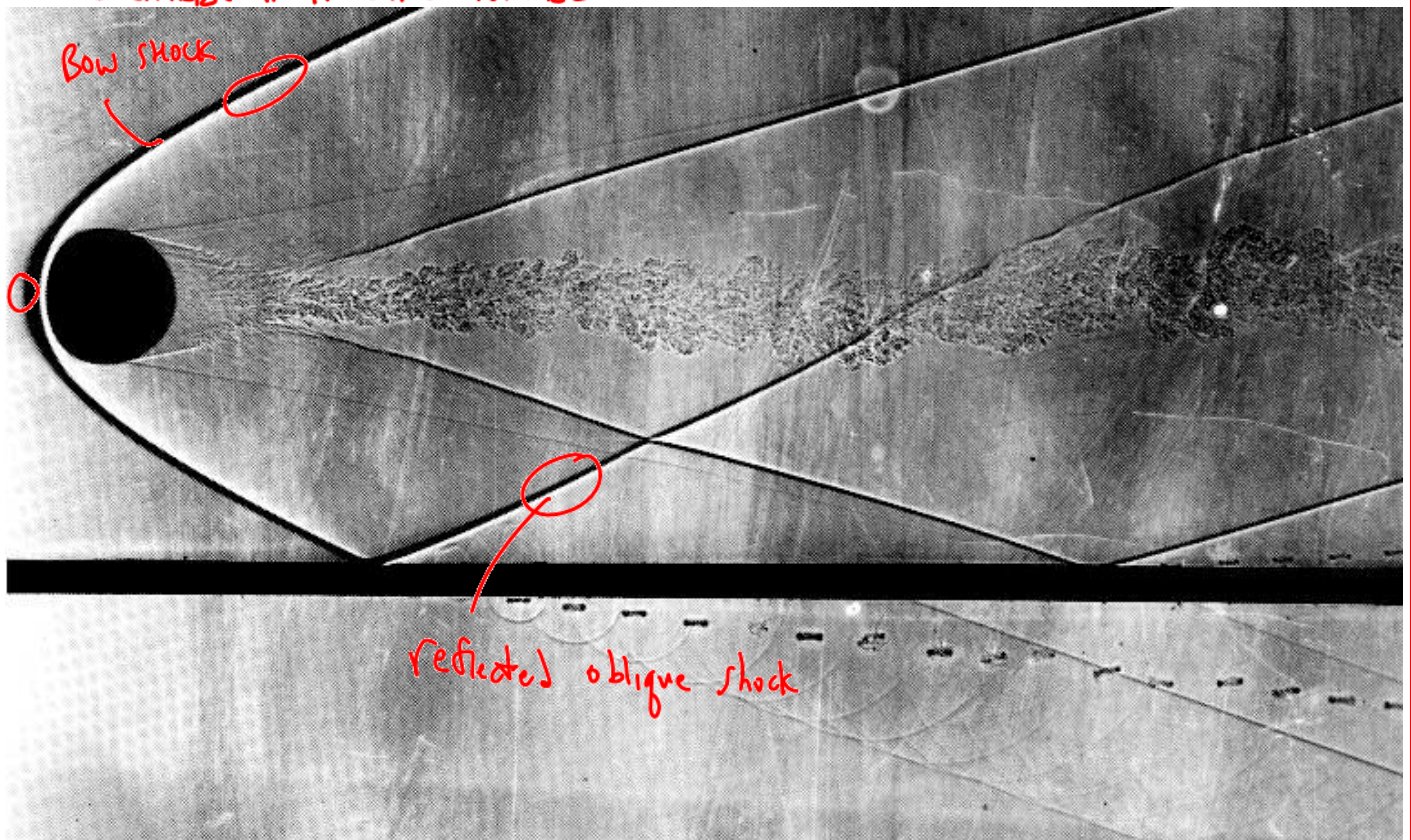
Bullets

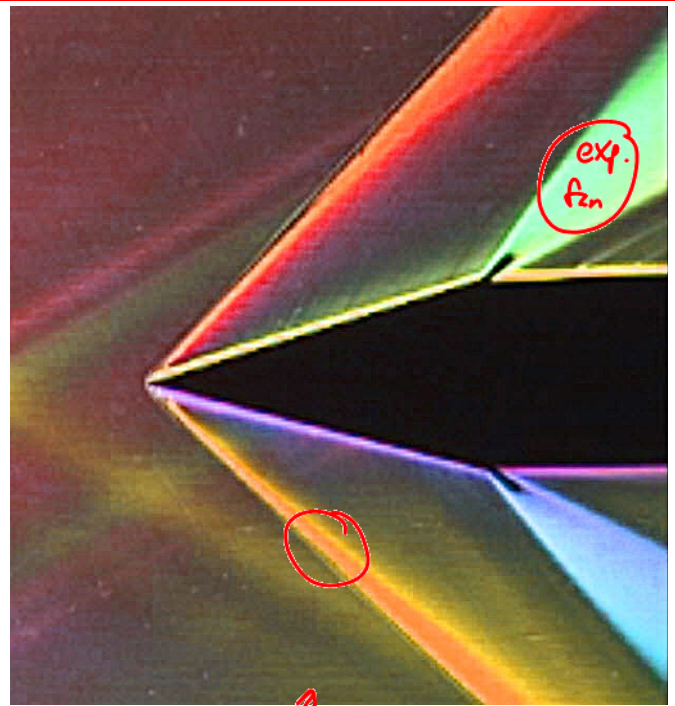
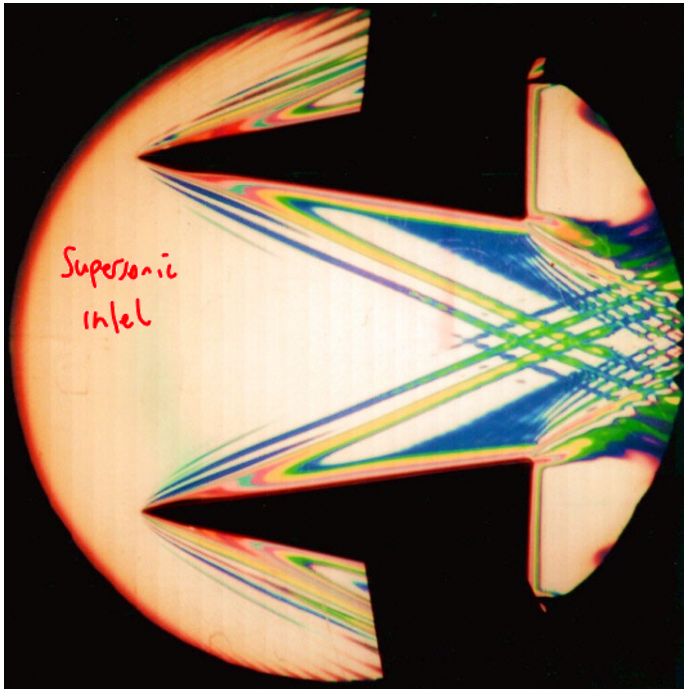


SUPERSONIC AIRCRAFT IN A WIND TUNNEL



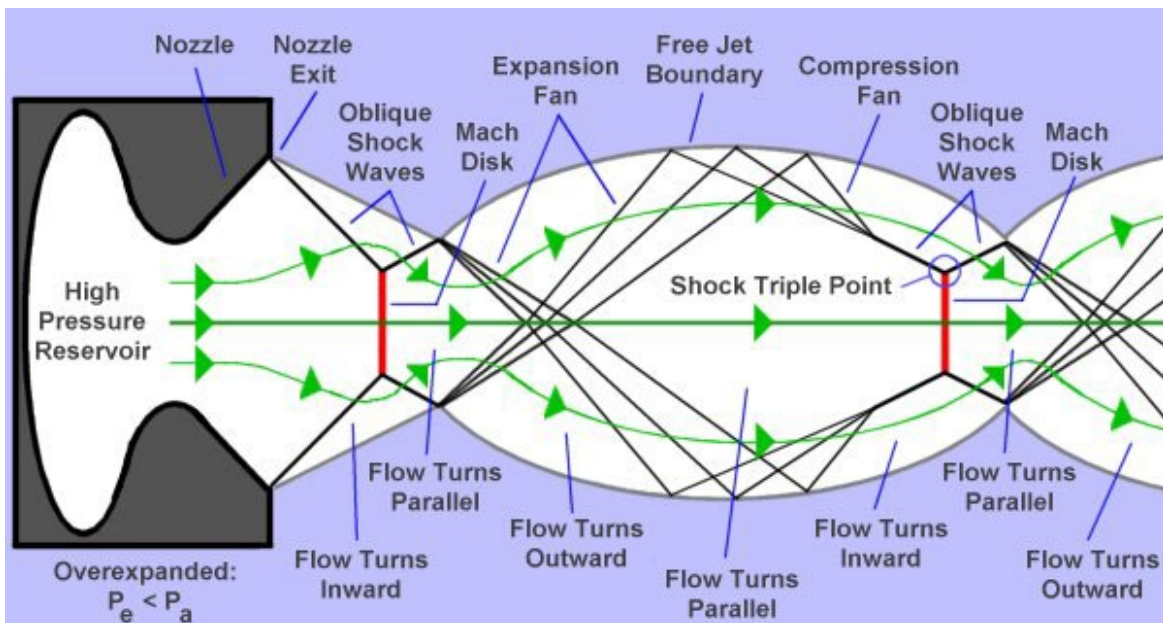
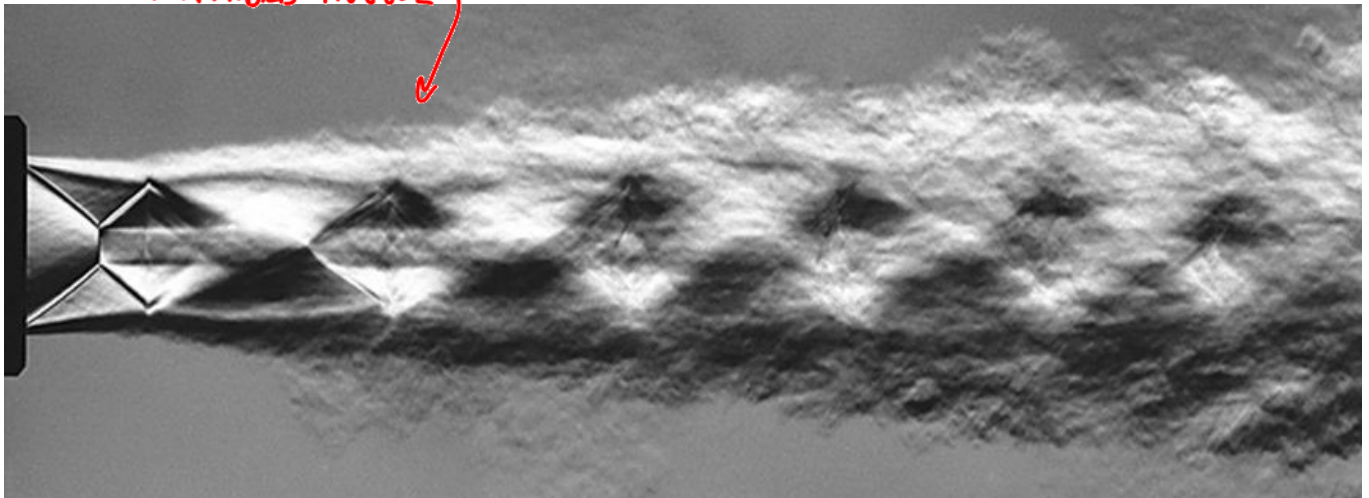
CYLINDER IN A WIND TUNNEL





OVEREXPANDED NOZZLE

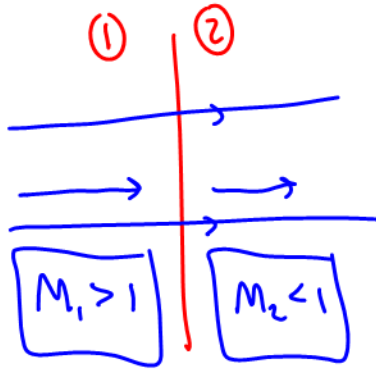
WEDGE FLOW



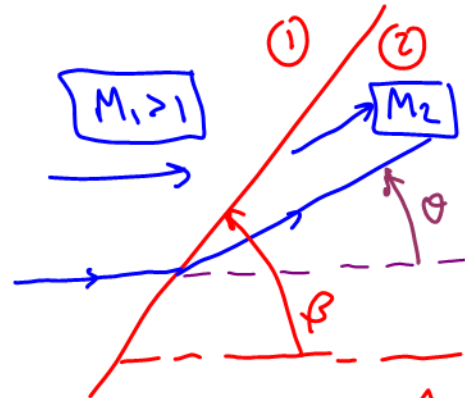
★ QUALITATIVE ANALYSIS OF OBLIQUE SHOCKS

A: A 2-D, ideal gas, ignore BLs on walls

NORMAL SHOCK



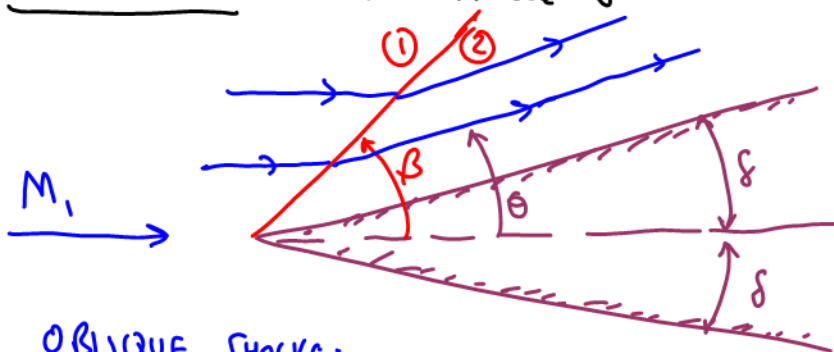
OBLIQUE SHOCK



$\beta =$ shock angle
 $\theta =$ turning angle

$M_2 < M_1$, M_2 can be < 1 or > 1

2-D WEDGE OF HALF-ANGLE δ



Here, $\theta = \delta$

$\theta =$ turning angle
 or deflection angle
 $\beta =$ shock angle
 $\delta =$ wedge half-angle

OBLIQUE SHOCKS:

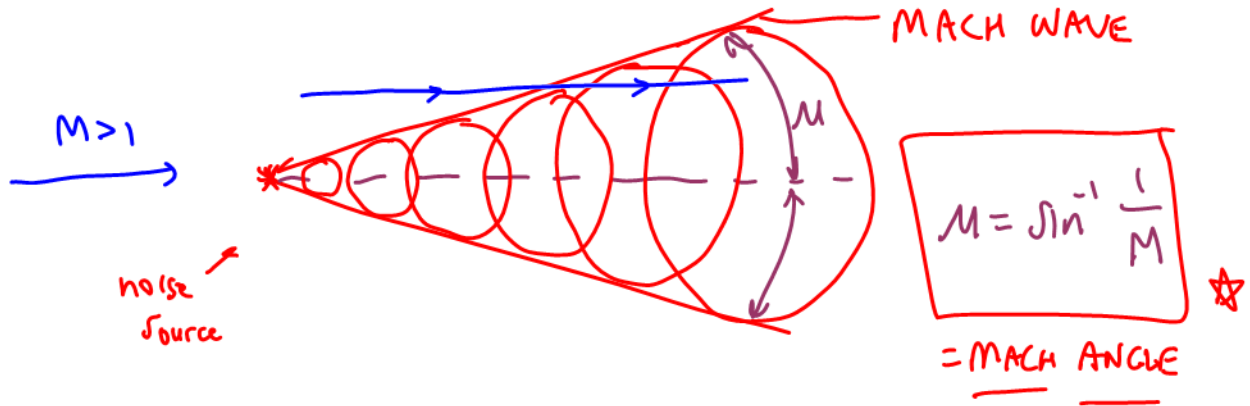
- Similar overall behavior as normal shocks

$$P_2 > P_1 \quad T_2 > T_1 \quad \rho_2 > \rho_1 \quad S_2 > S_1$$

$$T_{01} = T_{02} \quad P_{02} < P_{01} \quad M_2 < M_1$$

- **ALL OUR EQ'S FOR NORMAL SHOCKS STILL APPLY BUT WE MUST ACCOUNT FOR THE ANGLES**

RECALL, SOUND WAVE IN SUPERSONIC FLOW

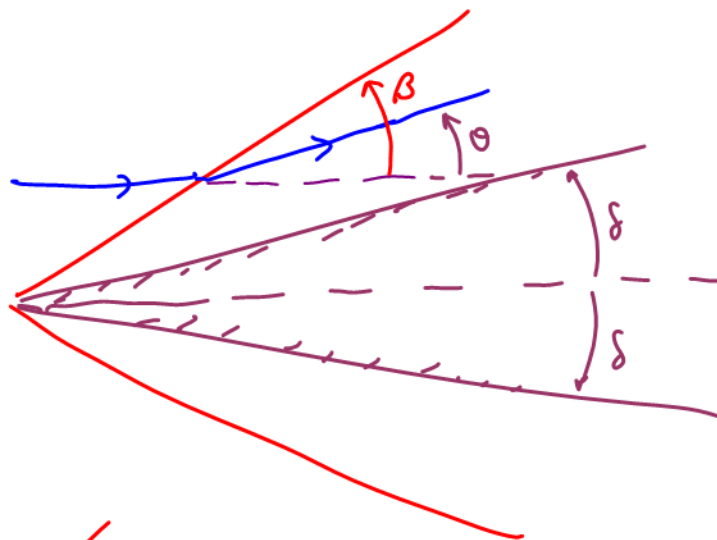


A MACH WAVE IS AN INFINITESIMALLY WEAK

- isentropic
- $\theta = \text{turning angle} = 0$
- $\beta = \mu$

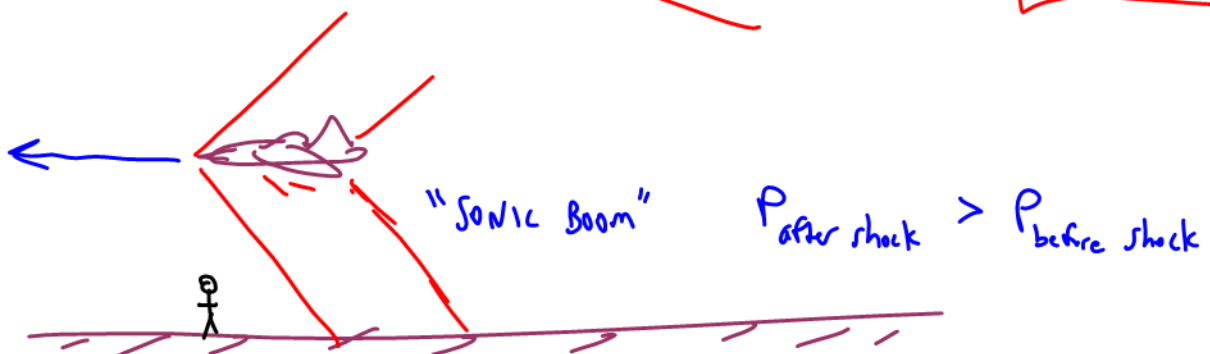
OBLIQUE SHOCK!

$M_1 = M_2$

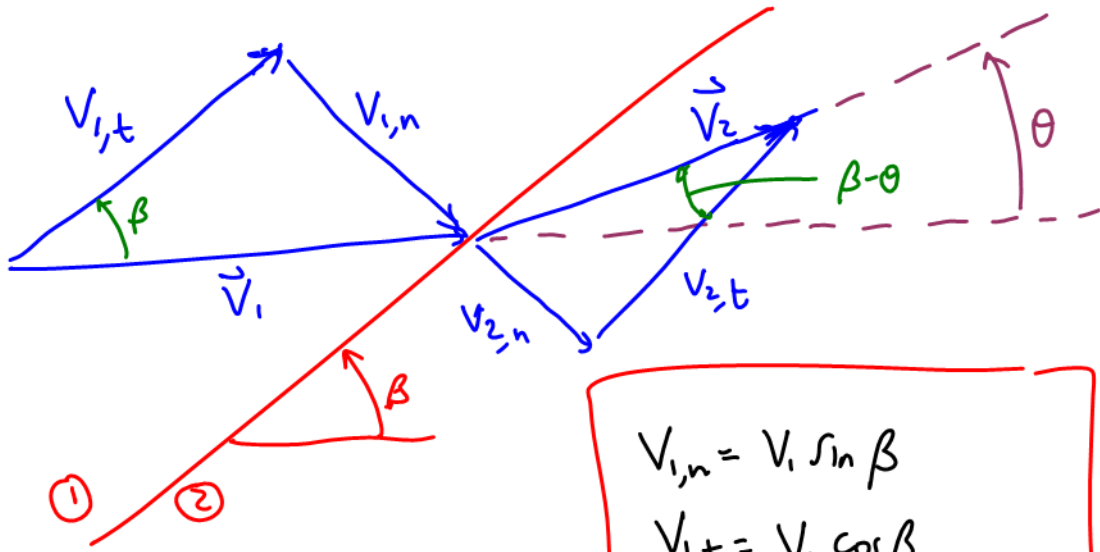


$\beta > M$

M is the lower limit of β



★ QUANTITATIVE ANALYSIS OF OBLIQUE SHOCK



① ②

KEY

$$V_{1,t} = V_{2,t} \quad \star$$

$$V_{1,n} = V_1 \sin \beta$$

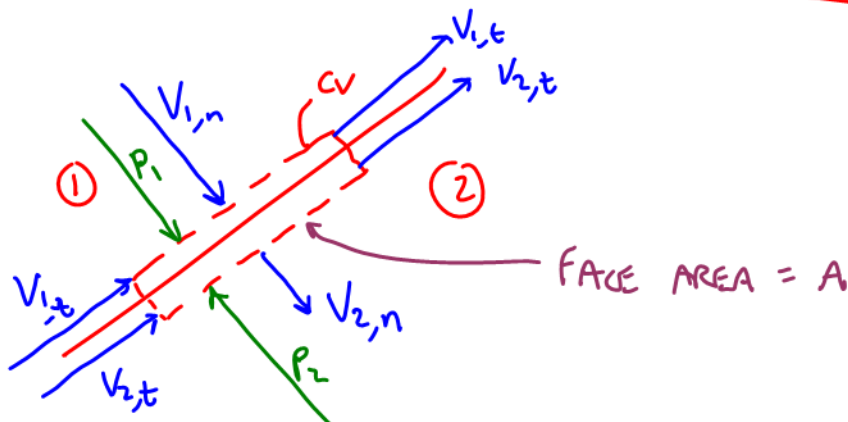
$$V_{1,t} = V_1 \cos \beta$$

$$V_{2,n} = V_2 \sin (\beta - \theta)$$

$$V_{2,t} = V_2 \cos (\beta - \theta)$$

★ THE TANGENTIAL COMPONENT OF THE OBLIQUE SHOCK IS NOT AFFECTED BY THE SHOCK!

★ Thus, our old normal shock eq's still apply, but in terms of the NORMAL component of velocity (Not V_1 , but $V_{1,n}$)



CONS. OF MASS:

$$\rho_1 V_{1,n} A = \rho_2 V_{2,n} A$$

$$\rho_1 V_{1,n} = \rho_2 V_{2,n} \quad (1)$$

MOMENTUM EQ:

- In tangential direction, nothing changes
- In normal direction,

$$\begin{aligned} P_1 A - P_2 A &= \sum_{\text{out}} \dot{m} V_n - \sum_{\text{in}} \dot{m} V_n \\ &= \rho_2 V_{2,n} A V_{2,n} - \rho_1 V_{1,n} A V_{1,n} \end{aligned}$$

$$\star P_1 - P_2 = \rho_2 V_{2,n}^2 - \rho_1 V_{1,n}^2 \quad (2)$$

CONS. OF ENERGY

$$h_{o1} = h_{o2}$$

or $T_{o1} = T_{o2}$
(ideal gas)

$$(h_o = h + \frac{1}{2} V^2)$$

\star (TOTAL VELOCITY MAGNITUDE)²

$$h_{o1} = h_1 + \frac{1}{2} V_{1,n}^2 + \frac{1}{2} V_{1,t}^2 = h_2 + \frac{1}{2} V_{2,n}^2 + \frac{1}{2} V_{2,t}^2 = h_{o2}$$

$$h_1 + \frac{1}{2} V_{1,n}^2 = h_2 + \frac{1}{2} V_{2,n}^2 \quad (3)$$

NORMAL SHOCK EQS

mass:

$$\rho_1 V_1 = \rho_2 V_2$$

mom:

$$P_1 - P_2 = \rho_2 V_2^2 - \rho_1 V_1^2$$

\Leftrightarrow

energy:

$$h_1 + \frac{V_1^2}{2} = h_2 + \frac{V_2^2}{2}$$

OBLIQUE SHOCK EQS

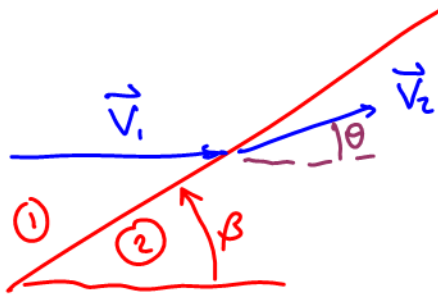
$$\rho_1 V_{1,n} = \rho_2 V_{2,n}$$

$$P_1 - P_2 = \rho_2 V_{2,n}^2 - \rho_1 V_{1,n}^2$$

$$h_1 + \frac{V_{1,n}^2}{2} = h_2 + \frac{V_{2,n}^2}{2}$$

EQS ARE IDENTICAL IF WE REPLACE V_1 BY $V_{1,n}$

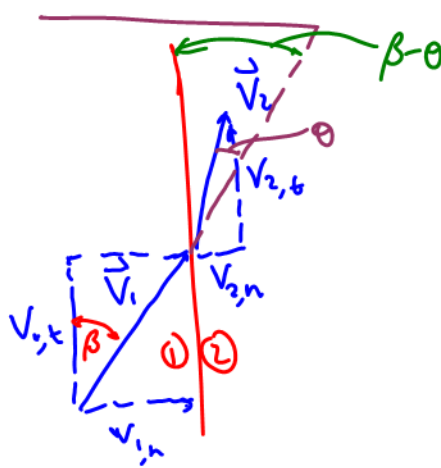
STATIONARY F.O.R.



$\therefore V_2$ BY $V_{2,n}$

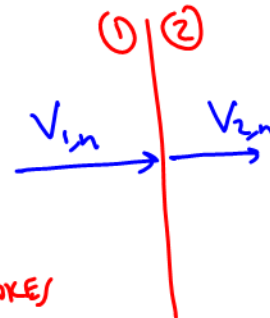
NOW ROTATE COUNTERCLOCKWISE
BY ANGLE $90^\circ - \beta$

ROTATED F.O.R.



ROTATED F.O.R.

\therefore MOVING UP @ SPEED
 $V_{1,t}$ (or $V_{2,t}$)



NOW IT LOOKS
LIKE A TYPICAL NORMAL SHOCK!

$$\text{Let } M_{1,n} = \frac{V_{1,n}}{a_1} = \frac{V_1}{a_1} \sin \beta \Rightarrow M_{1,n} = M_1 \sin \beta \quad (4)$$

$$M_{2,n} = \frac{V_{2,n}}{a_2} = \frac{V_2}{a_2} \sin(\beta - \theta) \Rightarrow M_{2,n} = M_2 \sin(\beta - \theta) \quad (5)$$

SO - WE USE THE SAME NORMAL SHOCK EQS WE USED BEFORE EXCEPT USE $M_{1,n}$ instead of M_1
 \vdots
 USE $M_{2,n}$ instead of M_2

e.g., $\frac{P_2}{P_1} = \text{fnc}(M_1, \gamma)$ For a normal shock

$\frac{P_2}{P_1} = \text{fnc}(M_{1,n}, \gamma)$ For an oblique shock

SAME EQ!

$M_{1,n}$ must be > 1 SUPERSONIC

$M_{2,n}$ must be < 1 SUBSONIC

BUT ACTUAL M_2 can be $<, =, > 1$