

## Equation Sheet for ME 522

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**Equation Sheet** for homework, Candy Friday questions, midterm exams, and the final exam.

- Two-dimensional boundary layer (BL) equations:** 
$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0, \quad u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = U \frac{dU}{dx} + \nu \frac{\partial^2 u}{\partial y^2}, \quad \frac{\partial p}{\partial y} = 0.$$

- Mangler's axisymmetric BL equations:** 
$$\frac{\partial(r_0 u)}{\partial x} + r_0 \frac{\partial v}{\partial y} = 0, \quad u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = U \frac{dU}{dx} + \nu \frac{\partial^2 u}{\partial y^2}, \quad \frac{\partial p}{\partial y} = 0.$$

- General axisymmetric BL equations:** 
$$\frac{\partial u_x}{\partial x} + \frac{1}{r} \frac{\partial}{\partial r}(r u_r) = 0, \quad u_x \frac{\partial u_x}{\partial x} + u_r \frac{\partial u_x}{\partial r} = U \frac{dU}{dx} + \frac{\nu}{r} \frac{\partial}{\partial r} \left( r \frac{\partial u_x}{\partial r} \right), \quad \frac{\partial p}{\partial r} = 0.$$

- The Mangler transformation:** 
$$x' = \frac{1}{L^2} \int_0^x r_0^2 dx, \quad y' = \frac{r_0 y}{L}, \quad u' = u, \quad U'(x') = U(x), \quad v' = \frac{L}{r_0} \left( v + \frac{dr_0}{dx} \frac{y u}{r_0} \right),$$

which yields an *equivalent 2-D flow* with BL equations: 
$$\frac{\partial u'}{\partial x'} + \frac{\partial v'}{\partial y'} = 0, \quad u' \frac{\partial u'}{\partial x'} + v' \frac{\partial u'}{\partial y'} = U' \frac{dU'}{dx'} + \nu \frac{\partial^2 u'}{\partial y'^2}.$$

- Three-dimensional boundary layers:**

**Scale factors or stretching factors:** For  $\bar{R} \equiv (X, Y, Z) = \bar{r}(x, z) + y\bar{n}(x, z)$ , 
$$h_x \equiv \left| \frac{d\bar{R}}{dx} \right| = \sqrt{\left( \frac{\partial X}{\partial x} \right)^2 + \left( \frac{\partial Y}{\partial x} \right)^2 + \left( \frac{\partial Z}{\partial x} \right)^2},$$

$$h_y \equiv \left| \frac{d\bar{R}}{dy} \right| = \sqrt{\left( \frac{\partial X}{\partial y} \right)^2 + \left( \frac{\partial Y}{\partial y} \right)^2 + \left( \frac{\partial Z}{\partial y} \right)^2}, \quad h_z \equiv \left| \frac{d\bar{R}}{dz} \right| = \sqrt{\left( \frac{\partial X}{\partial z} \right)^2 + \left( \frac{\partial Y}{\partial z} \right)^2 + \left( \frac{\partial Z}{\partial z} \right)^2}.$$
 **The 3-D BL equations:**

$$\frac{1}{h_x h_z} \left[ \frac{\partial}{\partial x}(h_z u) + \frac{\partial}{\partial z}(h_x w) \right] + \frac{\partial v}{\partial y} = 0, \quad \frac{u}{h_x} \frac{\partial u}{\partial x} + \frac{w}{h_z} \frac{\partial u}{\partial z} + v \frac{\partial u}{\partial y} + \frac{uw}{h_x h_z} \frac{\partial h_x}{\partial z} - \frac{w^2}{h_x h_z} \frac{\partial h_z}{\partial x} = -\frac{1}{\rho h_x} \frac{\partial p}{\partial x} + \nu \frac{\partial^2 u}{\partial y^2}, \quad \frac{\partial p}{\partial y} = 0,$$

$$\frac{u}{h_x} \frac{\partial w}{\partial x} + \frac{w}{h_z} \frac{\partial w}{\partial z} + v \frac{\partial w}{\partial y} - \frac{u^2}{h_x h_z} \frac{\partial h_x}{\partial z} + \frac{uw}{h_x h_z} \frac{\partial h_z}{\partial x} = -\frac{1}{\rho h_z} \frac{\partial p}{\partial z} + \nu \frac{\partial^2 w}{\partial y^2}.$$

- Some complex variable definitions:** For real variable  $x$ ,  $e^{ix} = \cos x + i \sin x$ ,  $e^{-ix} = \cos x - i \sin x$ ,

$$\cosh(x) = \frac{e^x + e^{-x}}{2}, \quad \sinh(x) = \frac{e^x - e^{-x}}{2}. \quad \text{For complex variable } z = x + iy, \text{ the sine and cosine of } z \text{ are } \sin z = \frac{e^{iz} - e^{-iz}}{2i}$$

and  $\cos z = \frac{e^{iz} + e^{-iz}}{2}$ , and the hyperbolic functions are defined as  $\cosh(z) = \frac{e^z + e^{-z}}{2}$  and  $\sinh(z) = \frac{e^z - e^{-z}}{2}$ .

- Linear stability analysis:** Notation:  $\tilde{q} = Q + q$ , where  $\tilde{q}$  = total flow variable,  $Q$  = basic state, and  $q$  = disturbance. [For temperature and density, use  $\tilde{T} = \bar{T} + T'$  and  $\tilde{\rho} = \bar{\rho} + \rho'$ .] A variable with a hat like  $\hat{q}$  is an *amplitude*.

**Procedure:** Step 0: Eq. of motion  $\mathcal{D}(\tilde{q}) = 0$ . Step 1: Basic state  $\mathcal{D}(Q) = 0$ . Step 2: Add disturbance  $\mathcal{D}(Q + q) = 0$ . Step 3: Subtract basic state  $\mathcal{D}(Q + q) - \mathcal{D}(Q) = 0$ . Step 4: Linearize. Step 5: Solve linearized disturbance eq. for  $q$ . Step 6: Examine stability.

- Method of normal modes:**  $q(x, y, z, t) = \hat{q}(z) e^{ikx + ily + \sigma t}$  for wave disturbances in the  $x$  and/or  $y$  directions, where  $q$  is a disturbance quantity – typically  $u, v, w$ , and  $p$ , or sometimes disturbance stream function  $\psi$ , and  $\hat{q}$  is an amplitude.

**Exam 1 material ends here.**

- Stability of locally parallel flows:** Basic state:  $U = U(y)$ , and  $V = W = 0$  [flow in  $x$  direction only].

**Normal modes:**  $\psi(x, y, t) = \phi(y) e^{ik(x-ct)}$ , where  $\psi$  is the *disturbance stream function*,  $\phi(y)$  is the amplitude of the disturbance,  $k$  is the wave number, and  $c$  is the wave speed. In general,  $k$  and  $c$  may be complex.

This yields the **Orr-Sommerfeld equation:** 
$$(U - c)(\phi_{yy} - k^2 \phi) - U_{yy} \phi = \frac{1}{ik \text{Re}} [\phi_{yyy} - 2k^2 \phi_{yy} + k^4 \phi].$$

## Turbulence, the Final Frontier!

- Boussinesq total flow equations:**  $\frac{\partial \tilde{u}_i}{\partial x_i} = 0$ ,  $\left( \frac{\partial \tilde{u}_i}{\partial t} + \tilde{u}_j \frac{\partial \tilde{u}_i}{\partial x_j} \right) = -\frac{1}{\rho_0} \frac{\partial \tilde{p}}{\partial x_i} - g \delta_{i3} [1 - \alpha (\tilde{T} - T_0)] + \nu \frac{\partial^2 \tilde{u}_i}{\partial x_j \partial x_j}$ ,  
 $\frac{\partial \tilde{T}}{\partial t} + \tilde{u}_j \frac{\partial \tilde{T}}{\partial x_j} = \kappa \frac{\partial^2 \tilde{T}}{\partial x_j \partial x_j}$ . [Note: These eqs. include buoyancy, but we usually ignore gravitational effects.]
- Reynolds decomposition:**  $\tilde{q} = Q + q$ ,  $\tilde{u}_i = U_i + u_i$ ,  $\tilde{p} = P + p$ , etc. **Reynolds stress tensor:**  $RS \equiv -\rho \overline{u_i u_j}$ .
- Incompressible mean flow:** Continuity:  $\frac{\partial U_i}{\partial x_i} = 0$ , Momentum:  $\rho \left( \frac{\partial U_i}{\partial t} + U_j \frac{\partial U_i}{\partial x_j} \right) = -\frac{\partial P}{\partial x_i} + \frac{\partial}{\partial x_j} \left( \mu \frac{\partial U_i}{\partial x_j} - \rho \overline{u_i u_j} \right)$ ,  
 Mean Kinetic Energy Equation:  $\frac{D}{Dt} \left( \frac{1}{2} U_i^2 \right) = \frac{\partial}{\partial x_j} \left[ -\frac{P U_j}{\rho_0} + 2\nu U_i S_{ij} - \overline{u_i u_j U_i} \right] + \overline{u_i u_j} \frac{\partial U_i}{\partial x_j} - \frac{g}{\rho_0} \overline{\rho U_3} - 2\nu S_{ij} S_{ij}$ .
- Mean strain rate tensor:**  $S_{ij} \equiv \frac{1}{2} \left( \frac{\partial U_i}{\partial x_j} + \frac{\partial U_j}{\partial x_i} \right)$ . **Fluctuating strain rate tensor:**  $S'_{ij} \equiv \frac{1}{2} \left( \frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right)$ .
- Kinematic Reynolds stress transport equation:**  
 $\frac{D}{Dt} (\overline{u_i u_j}) = - \left( \overline{u_i u_k} \frac{\partial U_j}{\partial x_k} + \overline{u_j u_k} \frac{\partial U_i}{\partial x_k} \right) + \frac{p}{\rho} \left( \frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) - \frac{\partial}{\partial x_k} \left[ \overline{u_i u_j u_k} - \nu \frac{\partial (\overline{u_i u_j})}{\partial x_k} + \frac{p}{\rho} (\overline{u_i \delta_{jk}} + \overline{u_j \delta_{ik}}) \right] - 2\nu \frac{\partial u_i}{\partial x_k} \frac{\partial u_j}{\partial x_k}$ .
- Turbulent kinetic energy per unit mass (t.k.e.):**  $q^2 = k = K \equiv \frac{1}{2} \overline{u_i u_i}$ . [I will use  $K$  for these equations.]
- The tke equation:**  $\frac{D}{Dt} (K) = \frac{\partial}{\partial x_j} \left[ -\frac{1}{\rho_0} \overline{p u_j} - \frac{1}{2} \overline{u_i^2 u_j} + 2\nu u_i S'_{ij} \right] - \overline{u_i u_j} \frac{\partial U_i}{\partial x_j} + g \alpha \overline{w T'} - 2\nu \overline{S'_{ij} S'_{ij}}$ .
- Turbulent Re:**  $R_\ell \sim \frac{u' \ell}{\nu}$ . **Kolmogorov microscales:**  $\nu \sim (\nu \varepsilon)^{1/4}$ ,  $\eta \sim \left( \frac{\nu^3}{\varepsilon} \right)^{1/4}$ ,  $\tau \sim \left( \frac{\nu}{\varepsilon} \right)^{1/2}$ , where  $\varepsilon \sim \frac{u'^3}{\ell}$ .

### Exam 2 material ends here.

- Eddy viscosity model for a 2-D Boundary Layer type flow:**  $-\rho \overline{uv} = \mu_e \frac{dU}{dy}$  or  $-\overline{uv} = \nu_e \frac{dU}{dy}$ .
- Standard high Reynolds number form of the  $K$ - $\varepsilon$  turbulence model:**  
 $\frac{DK}{Dt} \equiv \frac{\partial K}{\partial t} + U_j \frac{\partial K}{\partial x_j} = \frac{\partial}{\partial x_j} \left( \frac{\nu_e}{\sigma_k} \frac{\partial K}{\partial x_j} \right) + \nu_e \left( \frac{\partial U_i}{\partial x_j} + \frac{\partial U_j}{\partial x_i} \right) \frac{\partial U_i}{\partial x_j} - \varepsilon$   $\nu_e = \frac{\mu_e}{\rho} = C_\mu \frac{K^2}{\varepsilon}$   
 $\frac{D\varepsilon}{Dt} \equiv \frac{\partial \varepsilon}{\partial t} + U_j \frac{\partial \varepsilon}{\partial x_j} = \frac{\partial}{\partial x_j} \left( \frac{\nu_e}{\sigma_\varepsilon} \frac{\partial \varepsilon}{\partial x_j} \right) + \frac{C_{\varepsilon_1} \nu_e \varepsilon}{K} \left( \frac{\partial U_i}{\partial x_j} + \frac{\partial U_j}{\partial x_i} \right) \frac{\partial U_i}{\partial x_j} - C_{\varepsilon_2} \frac{\varepsilon^2}{K}$ . The constants are  $\sigma_k = 1.0$ ,  $\sigma_\varepsilon = 1.3$ ,  
 $C_\mu = 0.09$ ,  $C_{\varepsilon_1} = 1.44$ , and  $C_{\varepsilon_2} = 1.92$ . The **Boussinesq eddy viscosity model** is  $-\rho \overline{u_i u_j} \approx -\frac{2}{3} \rho K \delta_{ij} + 2\mu_e S_{ij}$ .
- Approximate relations for a turbulent flat plate boundary layer:**  $C_f = \frac{2\tau_w}{\rho U^2} = 0.027 \text{Re}_x^{-1/7}$ ,  
 $C_D = \frac{2D}{\rho U^2 b x} = 0.031 \text{Re}_x^{-1/7}$ ,  $\frac{\delta}{x} = 0.16 \text{Re}_x^{-1/7}$ .
- Inner variables (wall variables) for BL, channel, and pipe flows:**  $\tau_w \equiv \mu \frac{dU}{dy} \Big|_w$ ,  $u^* \equiv \sqrt{\frac{\tau_w}{\rho}}$ ,  $u^+ = \frac{U}{u^*}$ ,  $y^+ \equiv \frac{y_w u^*}{\nu}$   
 where  $y_w$  is the distance from the wall ( $y_w = y$  for a BL;  $y_w = y + b$  for a channel).
- Viscous sublayer:**  $u^+ = y^+$ . **Log-law layer:**  $u^+ = \frac{1}{\kappa} \ln y^+ + B$  where  $\kappa = 0.40$  to  $0.41$ ,  $B$  (also called  $a$ ) =  $5.0$  to  $5.5$ .